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### 54 Aluminium alloys for nuclear apparatus.

57 Aluminium alloys having the following composition (%  
by weight):

- Mg 0.2-4.0%
- V 0.1-2.0%
- Si (in case) 0.05-1.0%
- other possible elements: total quantity less than  
1000 p.p.m.
- Al balance to 100%.

The use of said alloys in nuclear apparatus, in particular  
in the first wall of nuclear fusion reactors.

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#### ALUMINIUM ALLOYS FOR NUCLEAR APPARATUS

##### Background of the Invention

This invention relates to aluminium alloys possessing time-stable mechanical, physical and chemical characteristics suitable for their use in nuclear apparatus, in particular in the first wall of nuclear fusion reactors.

The first wall of a nuclear fusion reactor is known to require the use of materials able to withstand very critical operating conditions for a long period of time (up to 10 years), they being subjected to temperatures up to 350-400°C (with a minimum of 120°C), to neutron irradiation and to corrosion in very pure water.

Because of its low activity following neutron irradiation, pure aluminium might appear to be a material suitable for this purpose.

However, when in the pure state and especially when hot, this material has low mechanical properties and low corrosion resistance, insufficient for its use for the aforesaid application.

This deficiency of pure aluminium could be overcome by using its known commercial alloys containing additives such as Si, Zn, Cu, Mg, Fe, Ni, Cr, Mn and Zr.

However, most of said additives are unsuitable for the aforesaid application in that activation problems arise when under neutron irradiation.

The use of hyper-pure alloys containing conventional additives of low activity would leave the problem of hot corrosion resistance in very pure water unsolved.

Summary of the Invention

The object of the present invention is therefore to provide aluminium alloys having the necessary initial mechanical, physical and chemical characteristics for their use in nuclear apparatus, in particular in the first wall of nuclear fusion reactors, said alloys being also able to maintain said initial characteristics substantially stable with time during their use.

Said object is attained according to the present invention by aluminium alloys containing Mg in a quantity of between 0.2 and 4% by weight, V in a quantity of between 0.1 and 2.0% by weight, possibly Si in a quantity of between 0 and 1% by weight, and conventional impurities (such as Cu, Mn, Cr, Ti, Zn, Ni, B, Fe) in a total quantity of less than 1000 p.p.m. by weight, the balance to 100% being represented by Al.

Said alloys can be prepared by the known typical casting methods for Al alloys (fusion-produced alloys). In order to obtain the relative required semi-finished products, suitable known cycles are used comprising homogenisation, extrusion and/or rolling, and/or other plastic deformation processes which may be necessary, as known to experts of the art.

Said alloys according to the invention can also be prepared (in particular alloys containing Si) by the known powder technology method. In this case, a dispersed phase of  $Al_2O_3$  and/or  $Al_2O_3 \cdot MgO$  type can also be present.

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100Preferred Embodiments of the Invention

Preferred compositions for the alloys prepared by fusion according to the invention comprise 2.5-3% of Mg, 0.1-0.5% of V, possibly 0.05-0.2% of Si, and less than 150 p.p.m. of conventional impurities, the balance to 100% being Al (quantities expressed by weight). Preferred compositions for alloys prepared by powder metallurgy according to the invention comprise 0.2-1% of Mg, 0.2-1% of Si, 0.5-2% of V, and less than 150 p.p.m. of conventional impurities, the balance to 100% being Al (quantities expressed by weight). Alloys prepared by fusion are particularly suitable for maximum

operating temperatures of 150-200°C for the said wall, whereas powder-produced alloys are preferred for temperatures above 200°C and up to 350-400°C.

5 The examples given hereinafter by way of non-limiting illustration describe the alloys according to the present invention in greater detail.

Example 1

10 A billet is cast by the semi-continuous method from an Al-Mg-V alloy which on chemical analysis shows the following composition (quantities expressed as % by weight):

Mg 2.69%; V 0.11%; Fe 100 p.p.m.; Si 11 p.p.m.; Cu 10 p.p.m.; Mn 5 p.p.m.; Zn 2 p.p.m.; Ni 3 p.p.m.; Ti less than 1 p.p.m.; Al balance to 100%.

15 Said billet is homogenised for 15 hours at 400°C and 24 hours at 460°C, and is then extruded at 420°C to a diameter of 14 mm. From the extrusion obtained in this manner, samples of the required size are prepared by known methods for determining tensile, physical and creep behaviour characteristics (by ASTM procedures), these 20 characteristics being shown hereinafter (the known symbols R, Rp 0.2, A and  $\sigma$  being used to indicate respectively the ultimate tensile stress, 0.2% yield strength, ultimate elongation and breaking stress):

- Tensile characteristics:

25	Test temperature	R N/mm <sup>2</sup>	Rp 0.2 N/mm <sup>2</sup>	A %
	20°C	171	70	32.6
	100°C	173	74	31.8
	125°C	162	78	38.6
30	150°C	152	76	39.5

- Physical characteristics

- Electrical resistivity at -196°C: 1.890  $\mu\Omega$  cm
- Coefficient of linear expansion between 20 and 200°C: 26.2 MK<sup>-1</sup>

35 - Creep behaviour:

- 1) - Test temperature: 120°C

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- Test duration: 1000 hours
- $\sigma$   $85 \text{ N/mm}^2$
- 2) - Test temperature:  $200^\circ\text{C}$
- Test duration: 1000 hours
- 5 -  $\sigma$   $62 \text{ N/mm}^2$

### Example 2

10 The procedure of Example 1 is followed, the only difference being that the alloy composition is as follows (quantities expressed in % by weight): Mg 2.68%; V 0.21%; Fe 12 p.p.m.; Si 11 p.p.m.; Cu 10 p.p.m.; Mn 5 p.p.m.; Ni 3 p.p.m.; Zn 2 p.p.m.; Ti less than 1 p.p.m.; Al balance to 100%.

The characteristics of said alloy are as follows:

- Tensile characteristics:

15	Test temperature	R	Rp 0.2	A
		$\text{N/mm}^2$	$\text{N/mm}^2$	%
	$20^\circ\text{C}$	172	74	30.1
	$100^\circ\text{C}$	170	80	28.9
	$125^\circ\text{C}$	161	80	34.0
20	$150^\circ\text{C}$	146	76	40.5

- Physical characteristics:

- Electrical resistivity at  $-196^\circ\text{C}$ :  $2.110 \mu\Omega \text{ cm}$
- Coefficient of linear expansion between 20 and  $200^\circ\text{C}$ :  $25.2 \text{ MK}^{-1}$

25 - Creep behaviour:

- Test temperature:  $120^\circ\text{C}$
- Test duration: 1000 hours
- $G$   $75 \text{ N/mm}^2$

### Example 3

30 Powdered Al (purity 99.99%), Mg, Si and V were used (in the weight proportions of Mg 0.97%, V 1.1%, Si 0.71%, Al balance to 100%) to prepare by the known powder metallurgy method a Al-Mg-Si-V alloy in the form of a billet of size 80 mm diameter x 200 mm, using the following main basic parameters: sintering temperature  $580^\circ\text{C}$ ; sintering time 24 hours; hot compacting at  $580^\circ\text{C}$  with a pressure

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of 550 N/mm<sup>2</sup>; billet extrusion at 450°C to a diameter of 10 mm; solution heat-treatment for 2 hours at 520°C; rapid quenching followed by ageing at 150°C for 15 hours.

On chemical analysis, said extruded billet shows the following composition (% by weight): Mg 0.66%; V 1.07%; Si 0.65%; Fe 80 p.p.m.; Cu 12 p.p.m.; Mn 7 p.p.m.; Zn 3 p.p.m.; Ni 2 p.p.m.; Ti less than 1 p.p.m.; Al balance to 100%.

The characteristics of said alloy are as follows:

- Tensile characteristics:

Test temperature	R N/mm <sup>2</sup>	Rp 0.2 N/mm <sup>2</sup>	A %
20°C	377	351	11
200°C	194	187	14
300°C	77	74	24

- Physical characteristics:

- Density: 2.71 Mg M<sup>-3</sup>
- Electrical resistivity at -196°C: 1.530  $\mu\Omega\text{-cm}$

The mechanical and physical characteristics of the three alloys described heretofore by way of example satisfy - as is apparent to an expert of the art - the requirements for their use in the primary wall of nuclear fusion reactors.

Moreover, said alloys have good resistance to corrosion in a moist environment, both at room temperature and under hot conditions (100-150°C), and in addition have excellent weldability by all the typical methods for aluminium, and good workability for producing semi-finished products, even of complex form.

From the foregoing description and examples, the alloys according to the invention are suitable for use in nuclear apparatus components, in particular in the first wall of nuclear fusion reactors, in accordance with the objects of the invention itself.

ALUMINIUM ALLOYS FOR NUCLEAR APPARATUS

CLAIMS

1. Aluminium alloys characterised by the following composition (component quantities expressed in % by weight):

5           - Mg from 0.2 to 4.0%  
          - V from 0.1 to 2.0%  
          - other possible components: total quantity less than  
          1000 p.p.m.  
          - Al **balance** to 100%

10           2. Aluminium alloys as claimed in claim 1, characterised by also containing Si in a quantity of between 0.05 and 1% by weight.

15           3. Aluminium alloys as claimed in claim 2, wherein the Si quantity is between 0.4 and 0.8% by weight.

4. Aluminium alloys as claimed in claim 1, wherein the component quantities (expressed in % by weight) are:

20           - Mg from 2.5 to 3.0%  
          - V from 0.1 to 0.5%  
          - other possible components: total quantity less than  
          150 p.p.m.  
          - Al **balance** to 100%

25           5. Aluminium alloys as claimed in claims 1 and 2, wherein the component quantities (expressed as % by weight) are:

          - Mg from 0.2 to 1%  
          - V from 0.5 to 2%  
          - Si from 0.2 to 1%  
30           - other possible components: total quantity less than  
          150 p.p.m.  
          - Al **balance** to 100%

35           6. Use of aluminium alloys as claimed in claims 1 to 5 in components of apparatus which are subjected to neutron irradiation during their operation.

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7. Use of aluminium alloys as claimed in claims 1 to 5 in the  
first wall of nuclear fusion reactors.



DOCUMENTS CONSIDERED TO BE RELEVANT						
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 3)			
X	US-A-4 043 840 (SPERRY et al.) * Claims 1,3,5 *	1,2,4	C 22 C 21/06			
X	FR-A-1 034 260 (GLASER) * Abstract points 1-5; example 2	1,2				
X	US-A-3 236 632 (FOERSTER) * Claims 2,4; page 1, table 1, example 11 *	1,2				
A	US-A-1 903 842 (TITUS) * Claims 1,4 *	1				
A	FR-A- 808 156 (I.G. FARBENINDUSTRIE AG) * Abstract point 1; page 1, lines 33-55; page 2, lines 51-52 *	1	TECHNICAL FIELDS SEARCHED (Int. Cl. 3)			
	-----		C 22 C 21/06 C 22 C 21/00			
<p>The present search report has been drawn up for all claims</p> <table border="1"> <tr> <td>Place of search THE HAGUE</td> <td>Date of completion of the search 09-03-1984</td> <td>Examiner LIPPENS M.H.</td> </tr> </table>				Place of search THE HAGUE	Date of completion of the search 09-03-1984	Examiner LIPPENS M.H.
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<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons &amp; : member of the same patent family, corresponding document</p>						

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